

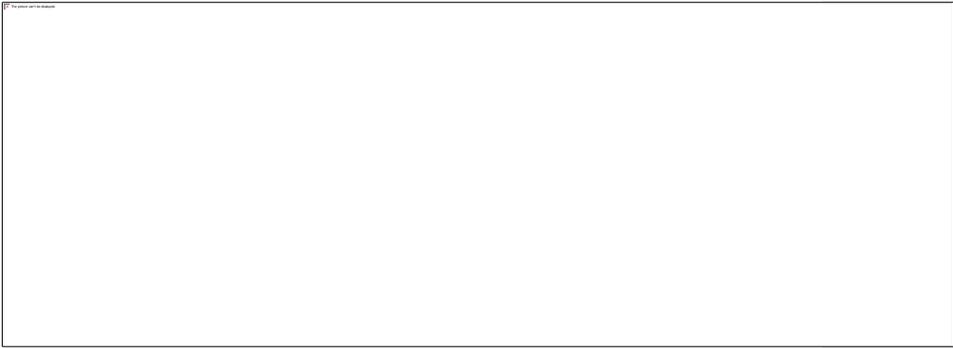
# Future inertia needs from a system split perspective

Jorrit Bos

System stability expert

11-02-2026





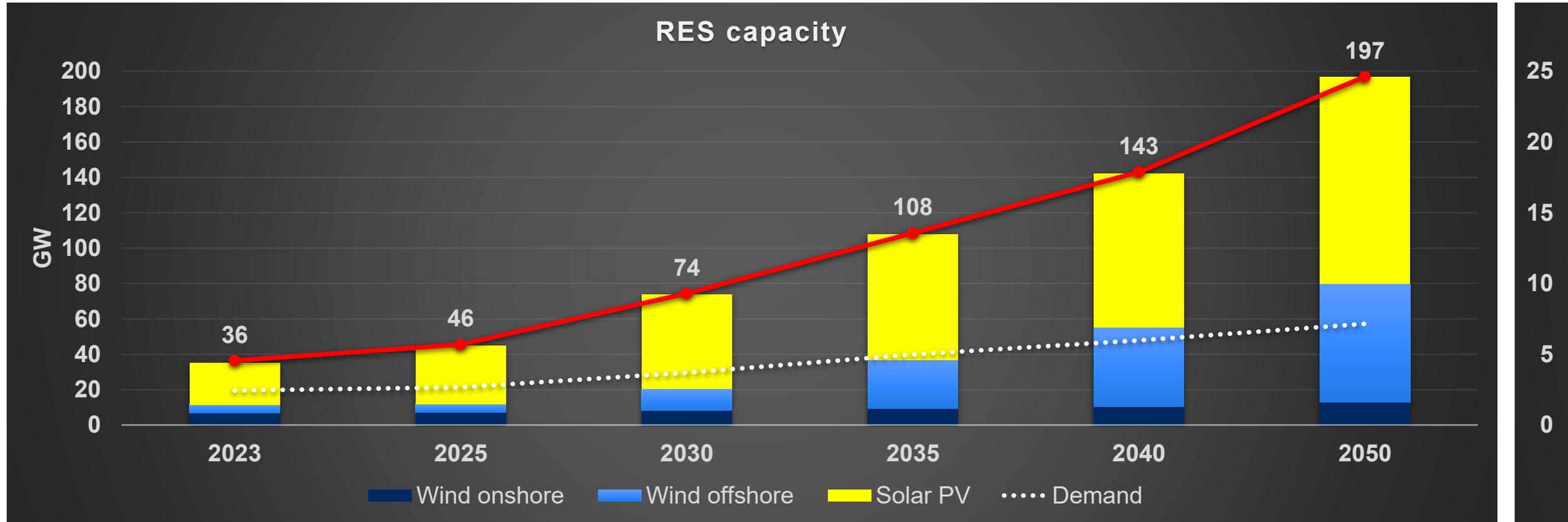
# Agenda

1. **Changing generation mix**
2. **System challenges – inertia**
3. **Inertia from Continental European perspective**
4. **Inertia developments in the Netherlands**



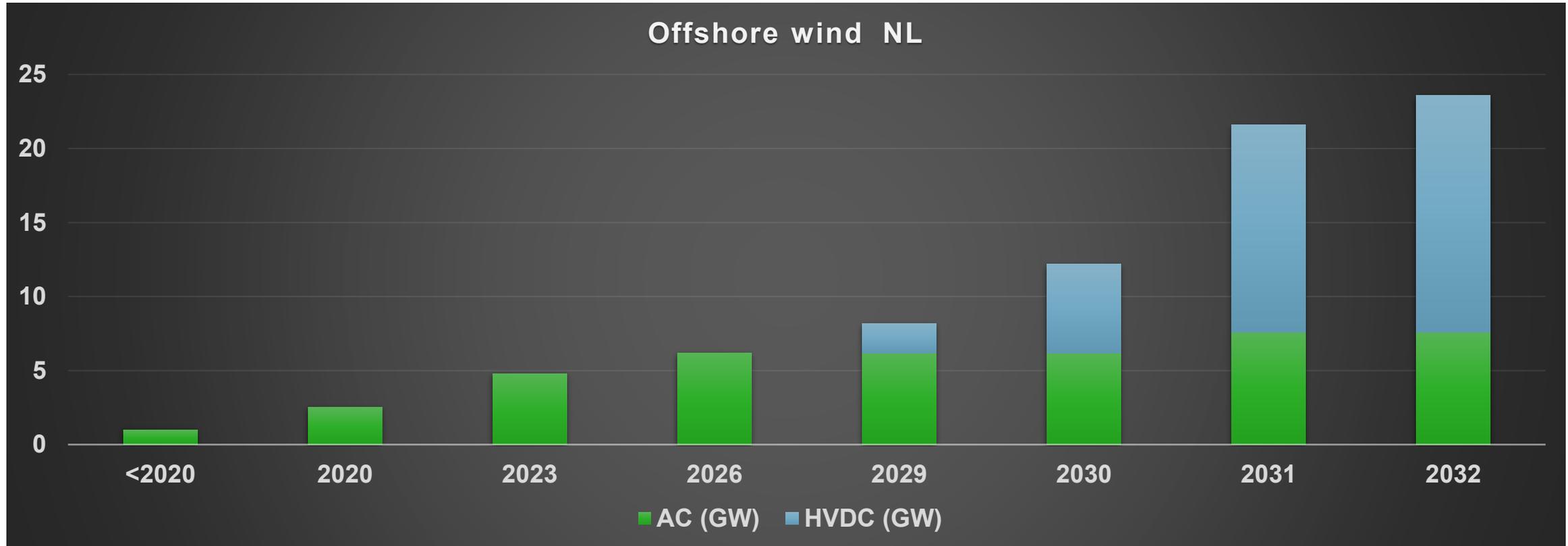
# Changing generation mix

# Installed capacity in the Netherlands



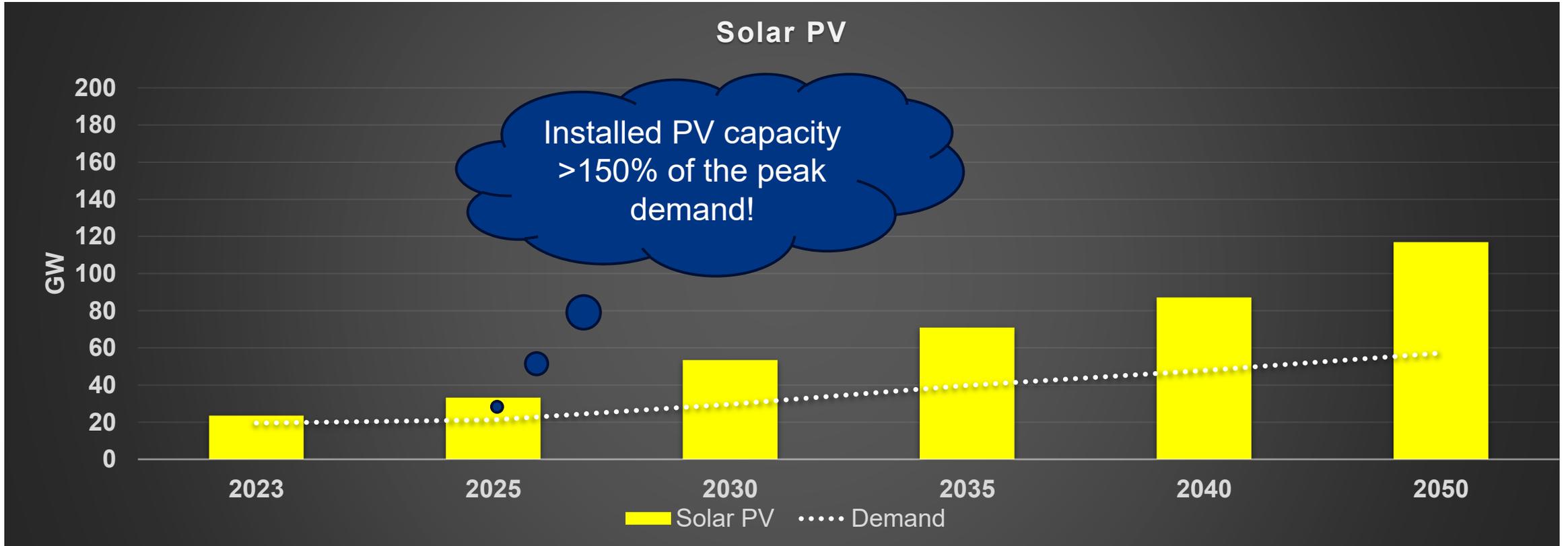
Graph based on data from TenneT IP2026 – KM scenario

# Installed capacity in the Netherlands



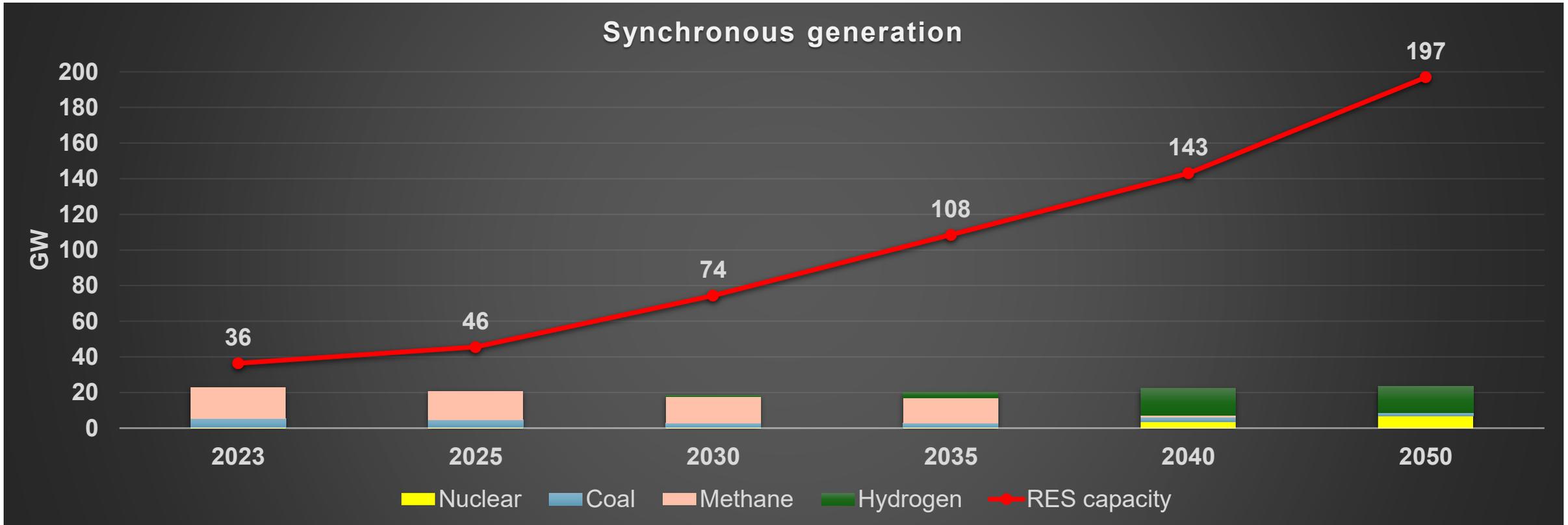
Graph based on data from TenneT IP2026 – KM scenario

# Installed capacity in the Netherlands

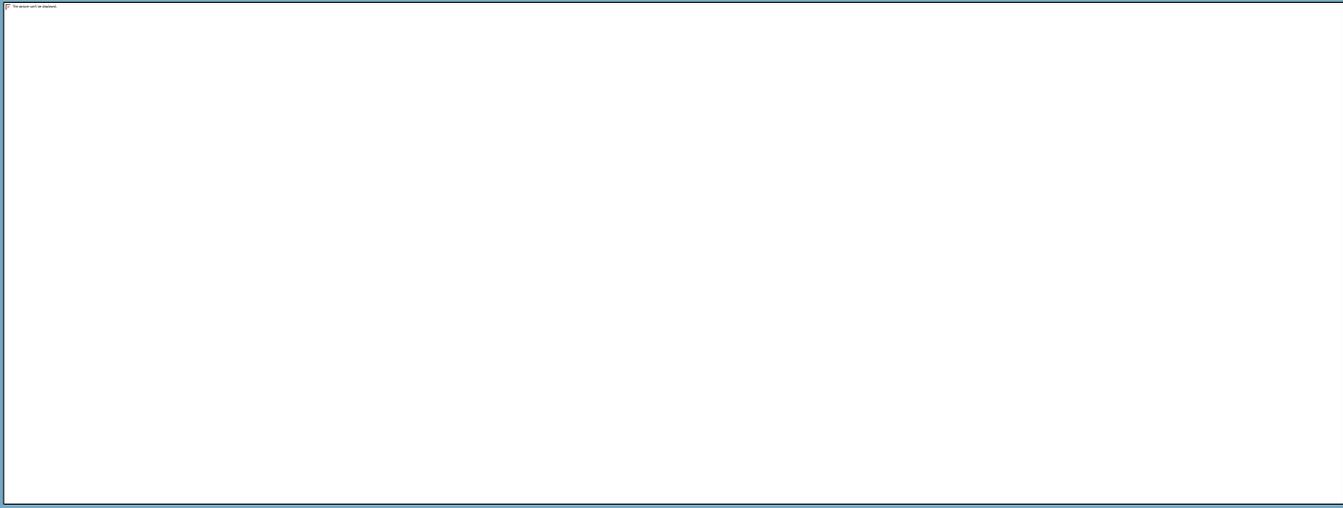


Graph based on data from TenneT IP2026 – KM scenario

# Installed capacity in the Netherlands

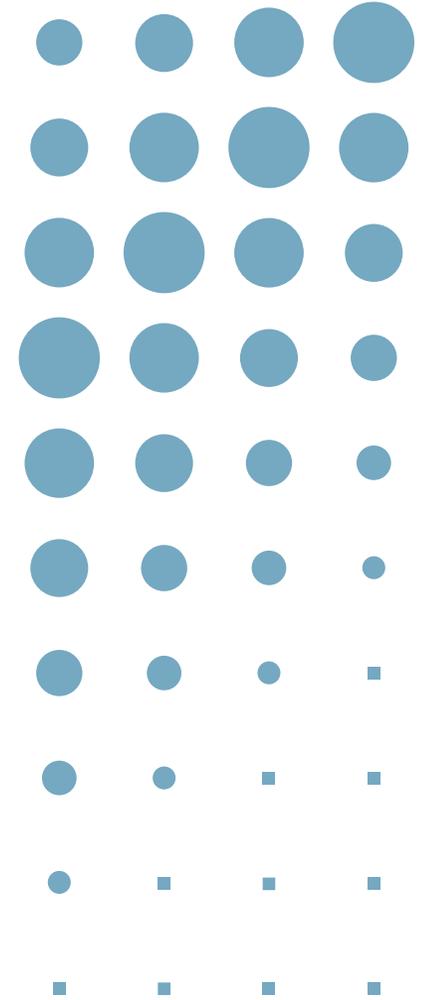
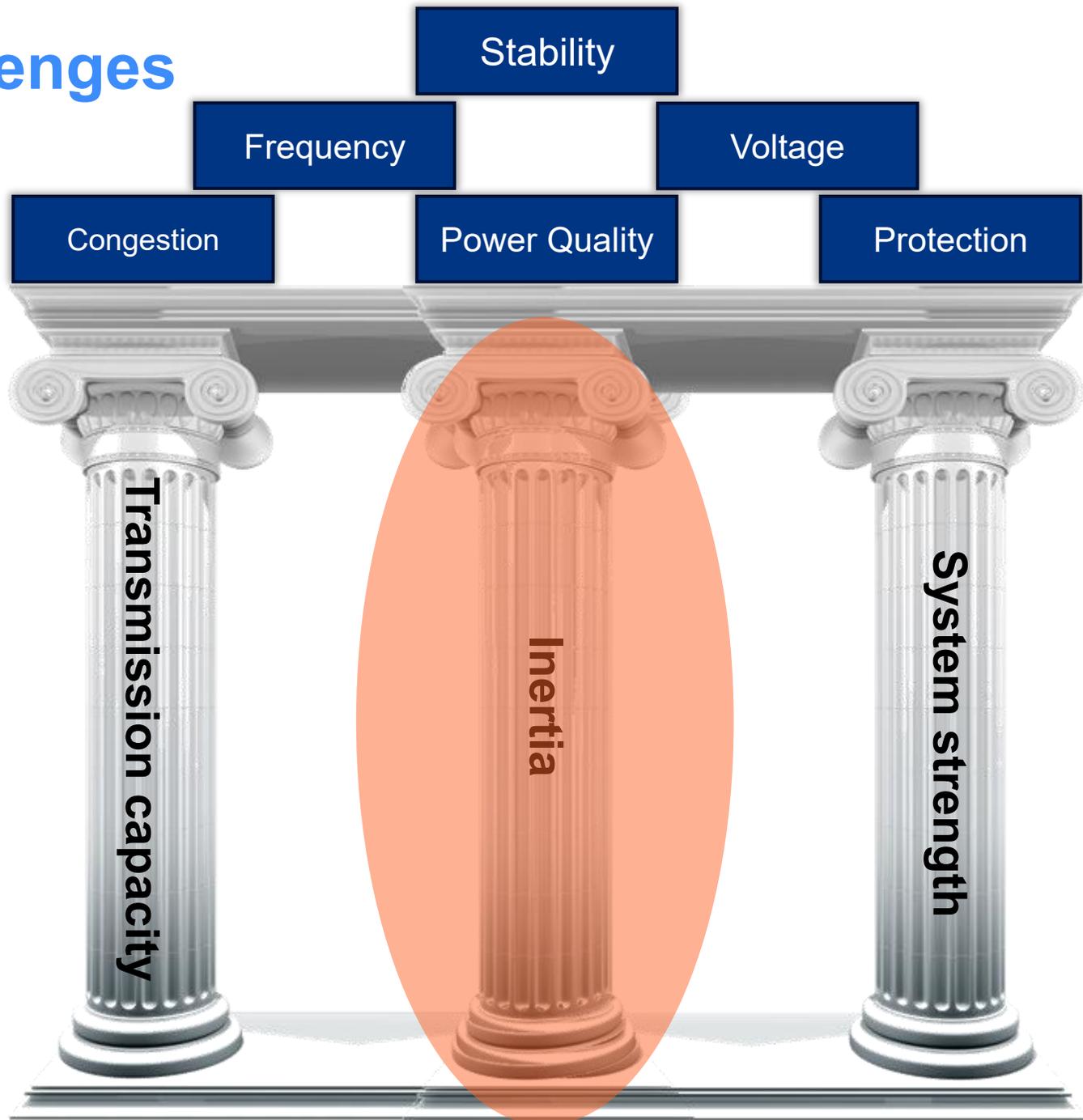


Graph based on data from TenneT IP2026 – KM scenario



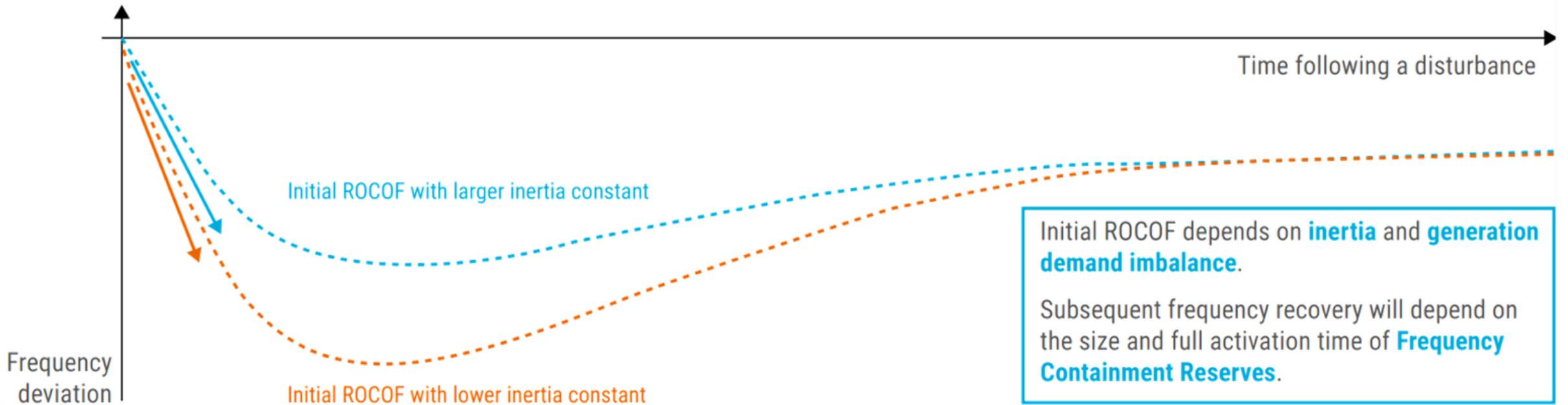
# System challenges - Inertia

# System challenges

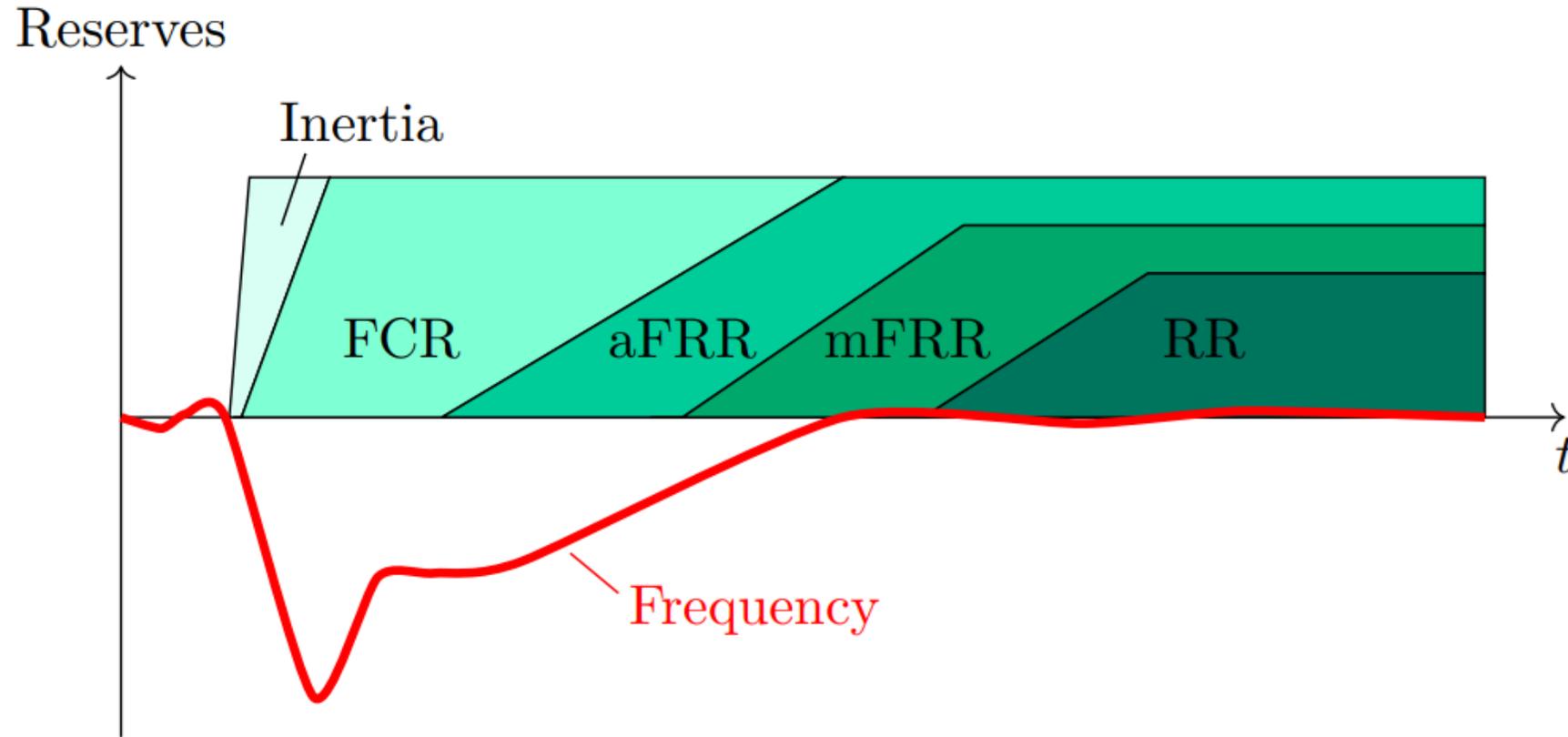


# Inertia – Why do we need it?

Inertia limits the speed at which the frequency changes; **RoCoF** (Rate of Change of Frequency)



# Inertia and frequency reserves - timescales



Reserve	Response time
Inertia	Instantaneous
Frequency Containment Reserves (FCR)	after 2 seconds
Automatic Frequency Restoration Reserves (aFRR)	30 seconds
Manual Frequency Restoration Reserves (mFRR)	5 min
Replacement Reserves (RR)	12,5 min

# Risks of increasing RoCoF

Current operational RoCoF limit  
is 1 Hz/sec<sup>1</sup>

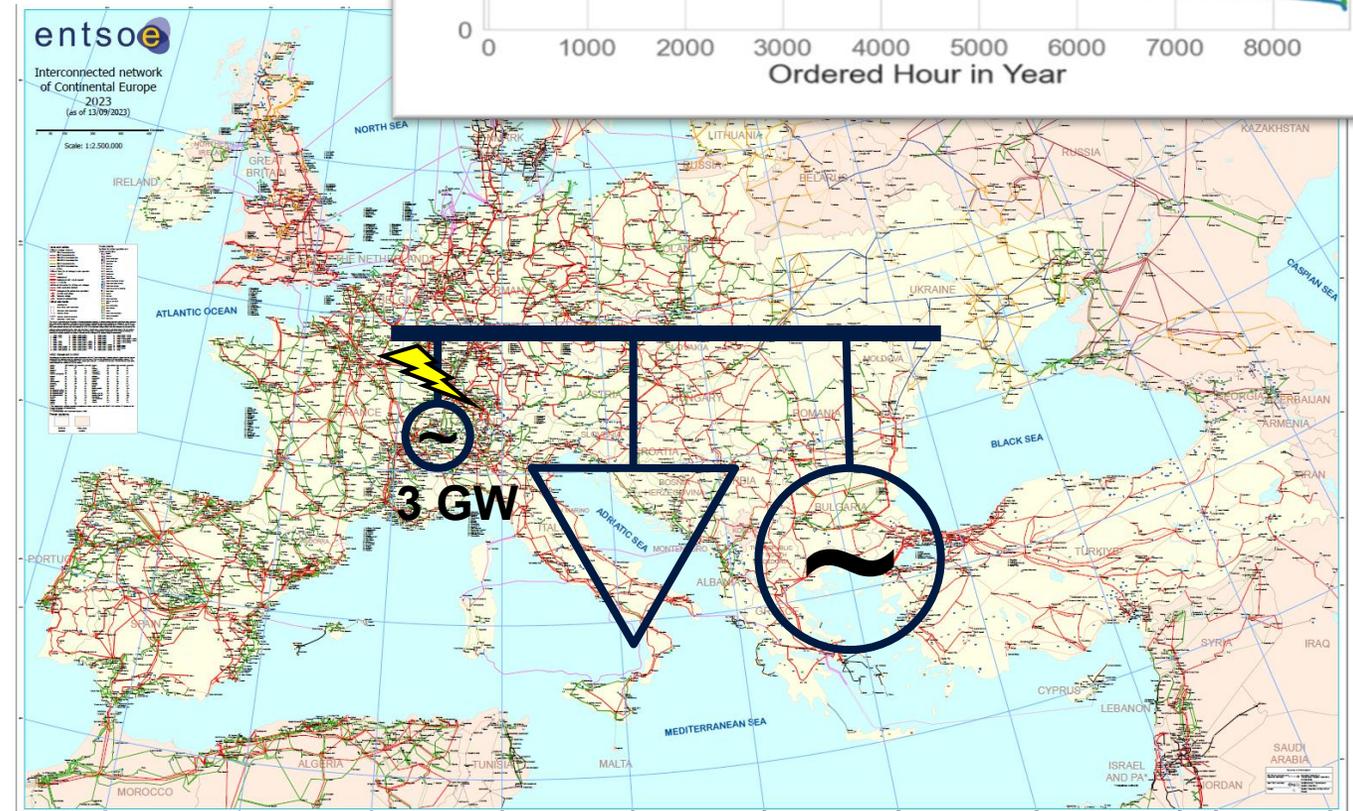
- **Mechanical stress in synchronous machines**
  - Resulting in failures/breakages
- **Misfunctioning low frequency demand disconnection (LFDD)**
  - Acts between 49-48Hz
  - Load is being shed in 6-10 tranches
  - Response time ~ 200 ms
  - → Risk of undershedding in case high RoCoF
- **Cascading effects risks, leading to a possible blackout**

# Inertia from Continental European perspective

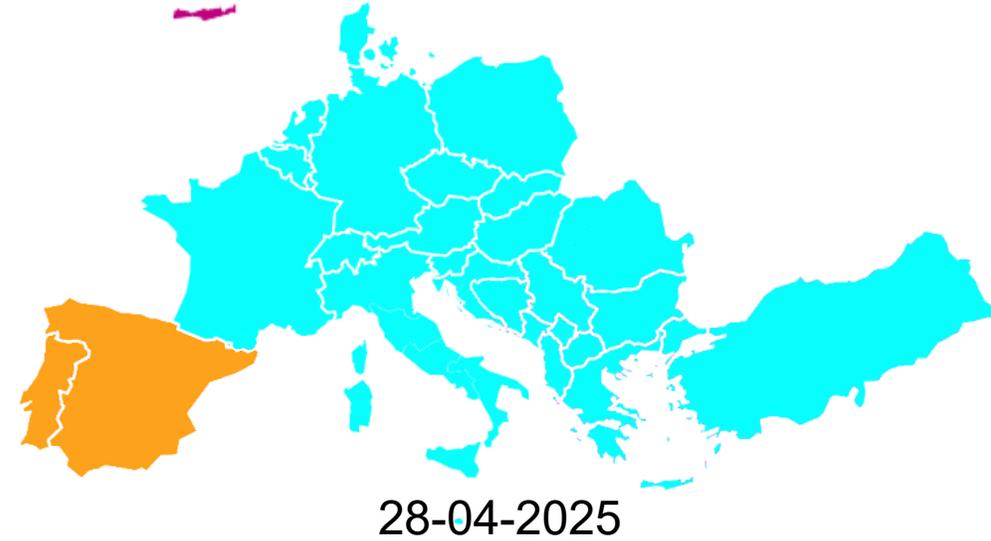
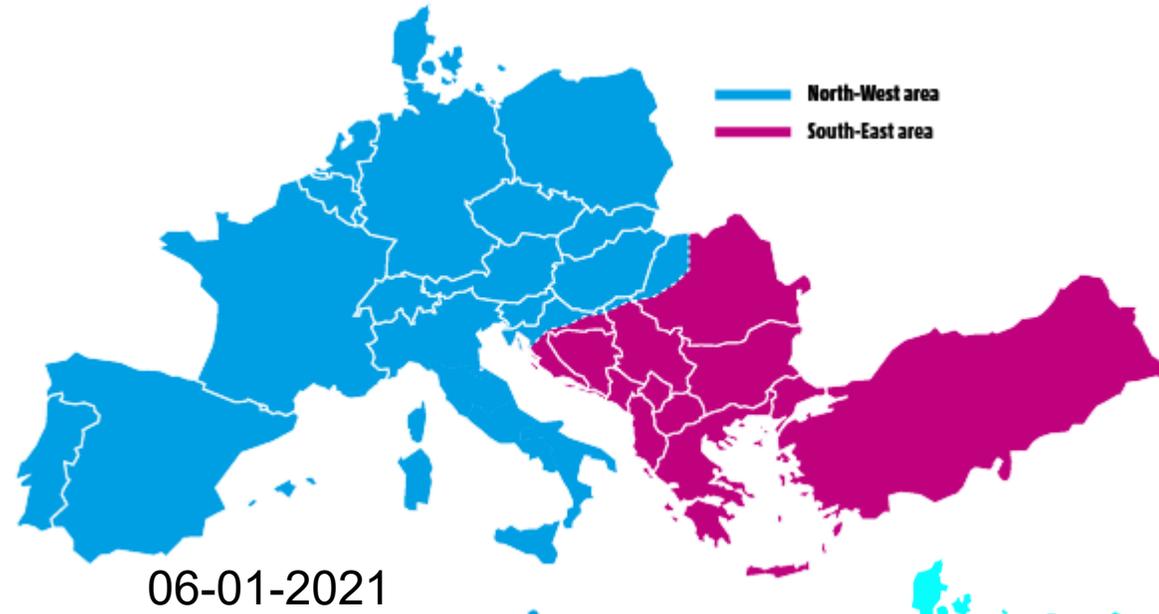
# Inertia - normal situation

## Interconnected system

- Reference-incident 3000 MW:
  - Frequency should stay  $>49,8$  Hz
  - No load disconnection
  - 'Automatic' recovery (primary control)
- Sum of inertia
  - Natural spread
  - Still 'quite some' inertia on system level
  - NL part of the big system

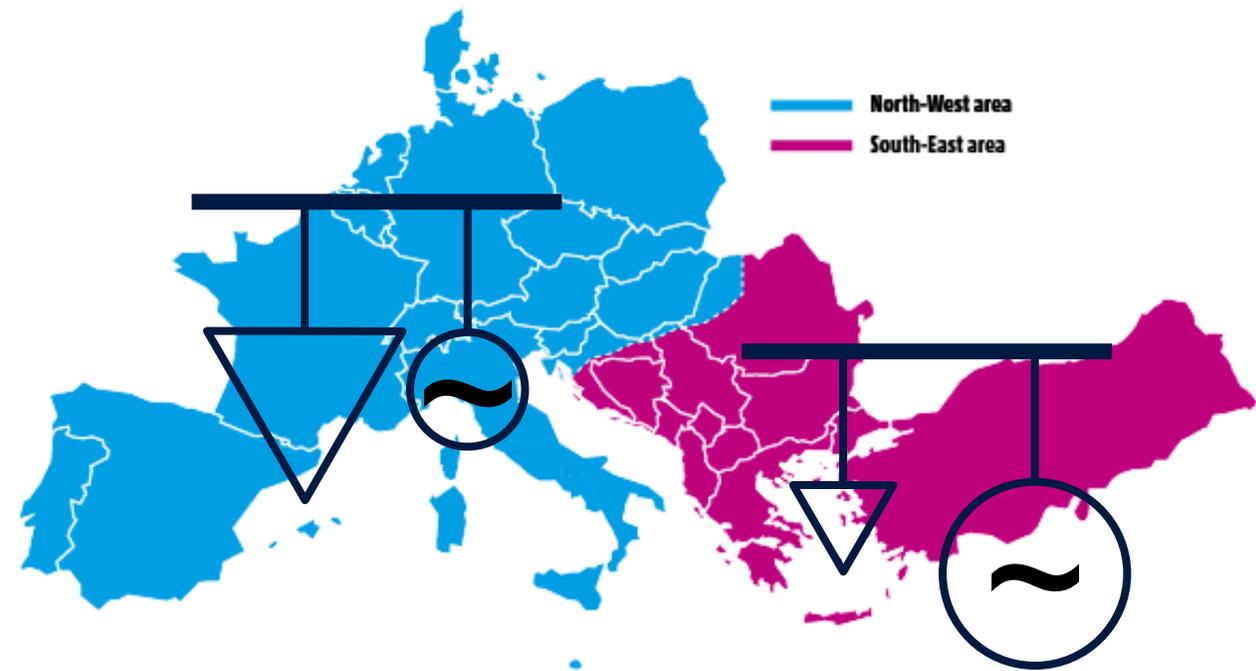


# Inertia - system splits examples



# Inertia - system splits (2)

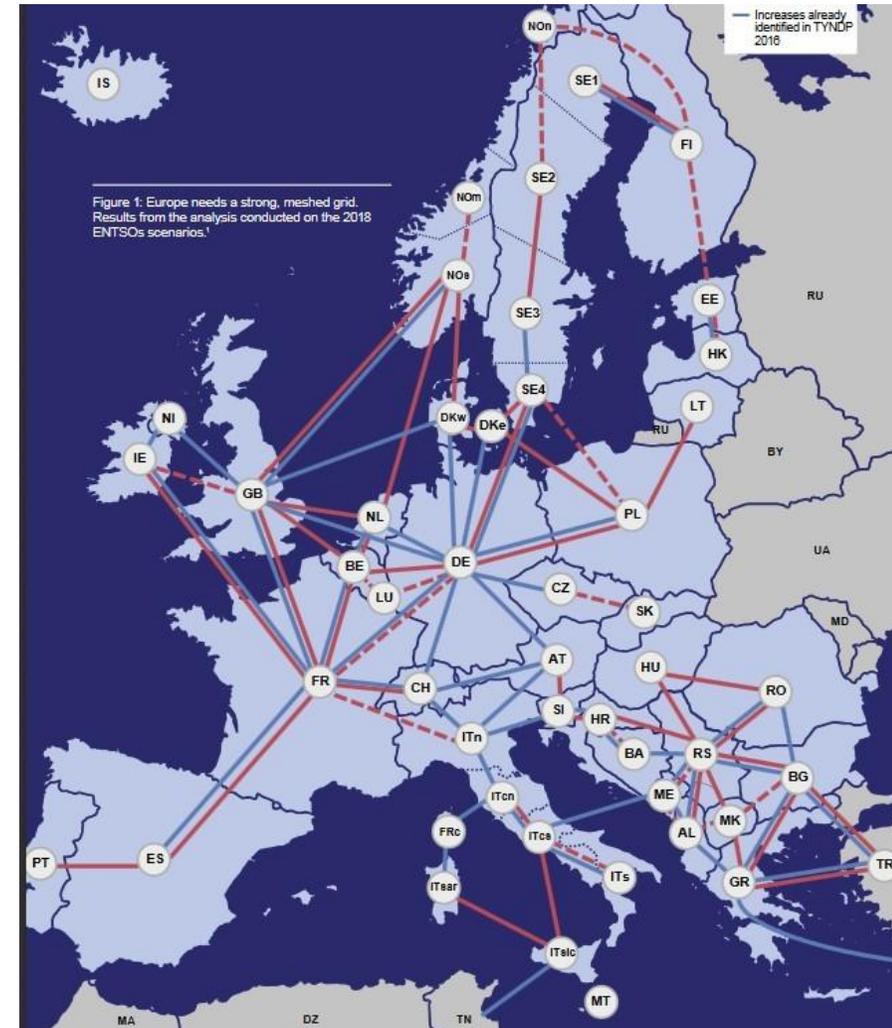
- Possible unbalance larger than reference-incident
  - Risk of black-out due to large unbalance and low inertia
- Theoretically every split possible
- In practice very low probability of NL island
- ENTSO-E 'project inertia'<sup>1</sup>
  - Identify inertia need per country



# ENTSO-E project inertia

## Calculation methodology and assumptions

- **Objective**, to calculate for system splits:
  - RoCoF (R)
  - Frequency response (F)
- **Inputs** from market simulations
  - Ten Year Network Development plan (TYNDP) 2022
- **Simplified model** of European grid:
  - one node per market zone, no impedance
  - Hourly data of generation mix and flows between market zones
  - 6 scenarios
  - Generic inertia data per fuel type and country



# Overview possible blackout cases

- Assessment of RoCoF and frequency nadir/zenith
- Assumed blackout in case:
  - $f < 47,5$  Hz
  - $f > 51,5$  Hz
  - $|\text{RoCoF}| > 1\text{Hz/s}$

<b>RR</b> Both areas: $ \text{RoCoF}  > 1\text{Hz/s}$	<b>FF</b> Both areas: $f < \text{ or } f >$	<b>RF</b> One area: $ \text{RoCoF}  > 1\text{Hz/s}$ Other area: $f < \text{ or } f >$	<b>Total blackout</b>
<b>R</b> One area: $ \text{RoCoF}  > 1\text{Hz/s}$	<b>F</b> One area: $f < \text{ or } f >$	<b>Partial blackout</b>	

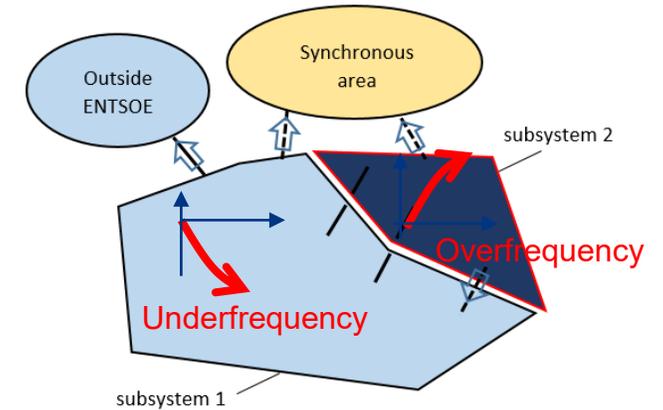
# Calculation of the RoCoF (R)

- No grid model
- Imbalance is assumed instantaneous
- RoCoF derived from rotating masses equation:

$$RoCoF(Hz/s) = \frac{df}{dt} = \frac{50Hz}{f_0} \frac{Imbalance (MW)}{2H_{eq} \sum Smax_{gen}}$$

*generation running capacity(MVA)*

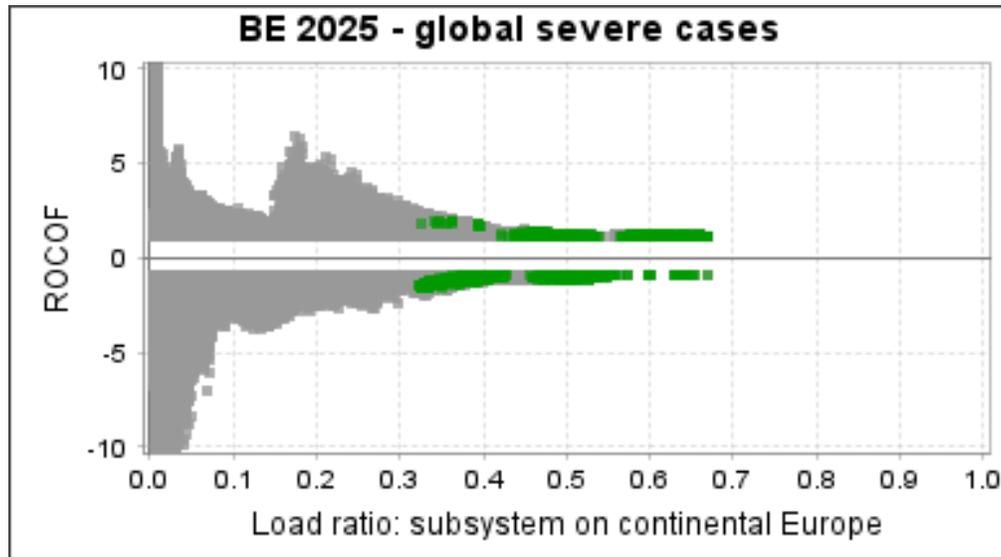
- RoCoF calculated at centre of inertia:  $H_{eq} = \frac{\sum H_{gen} Smax_{gen}}{\sum Smax_{gen}}$



Focus on 'global severe splits'

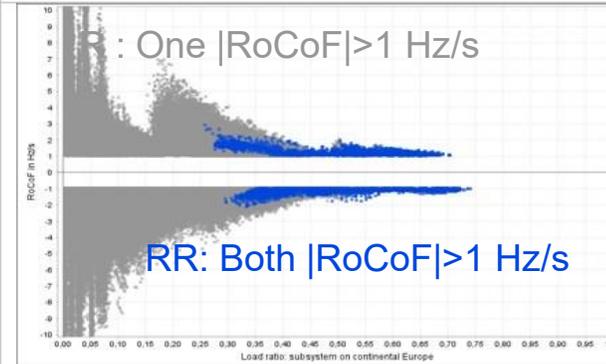
- |RoCoF| > 1Hz/s in both islands
- Beyond 1Hz/s frequency stability is not guaranteed
- Risk of blackout of the whole synchronous area

# Results RoCoF (R)

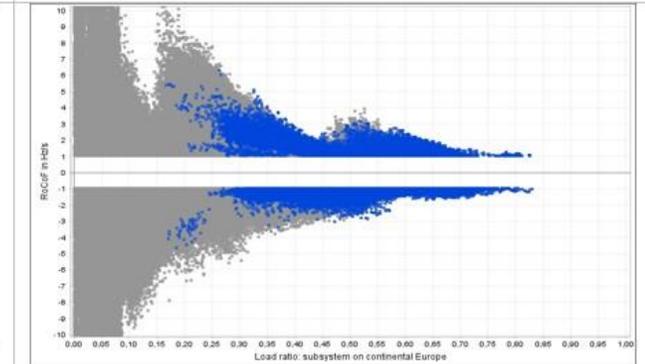


A clear degradation of the resilience of the system

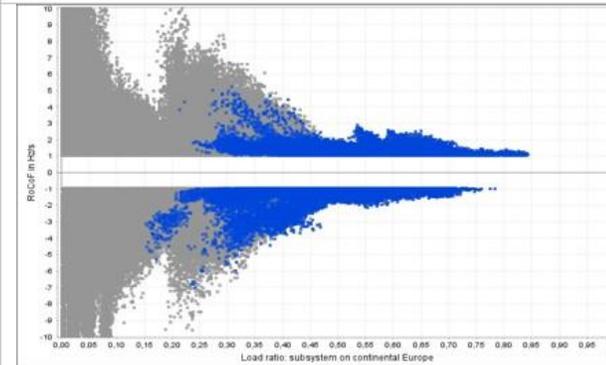
NT 2030



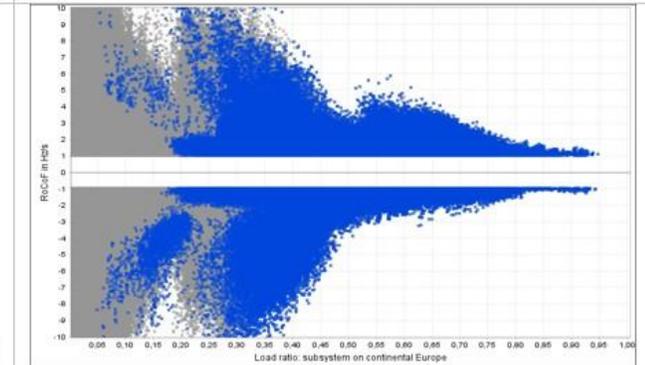
NT2040



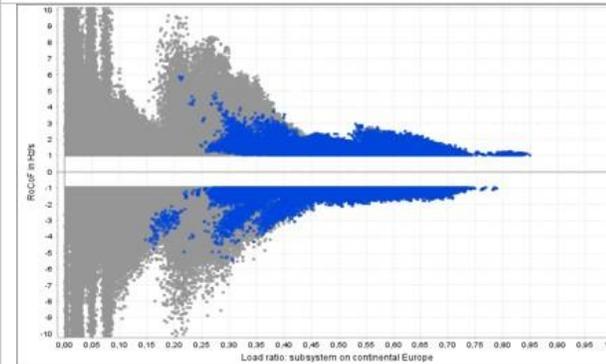
DE2030



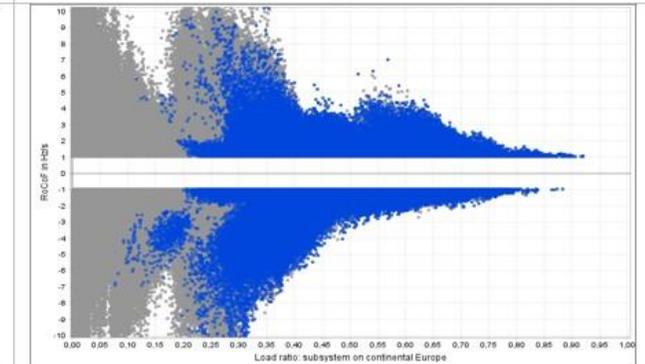
DE2040



GA2030



GA2040

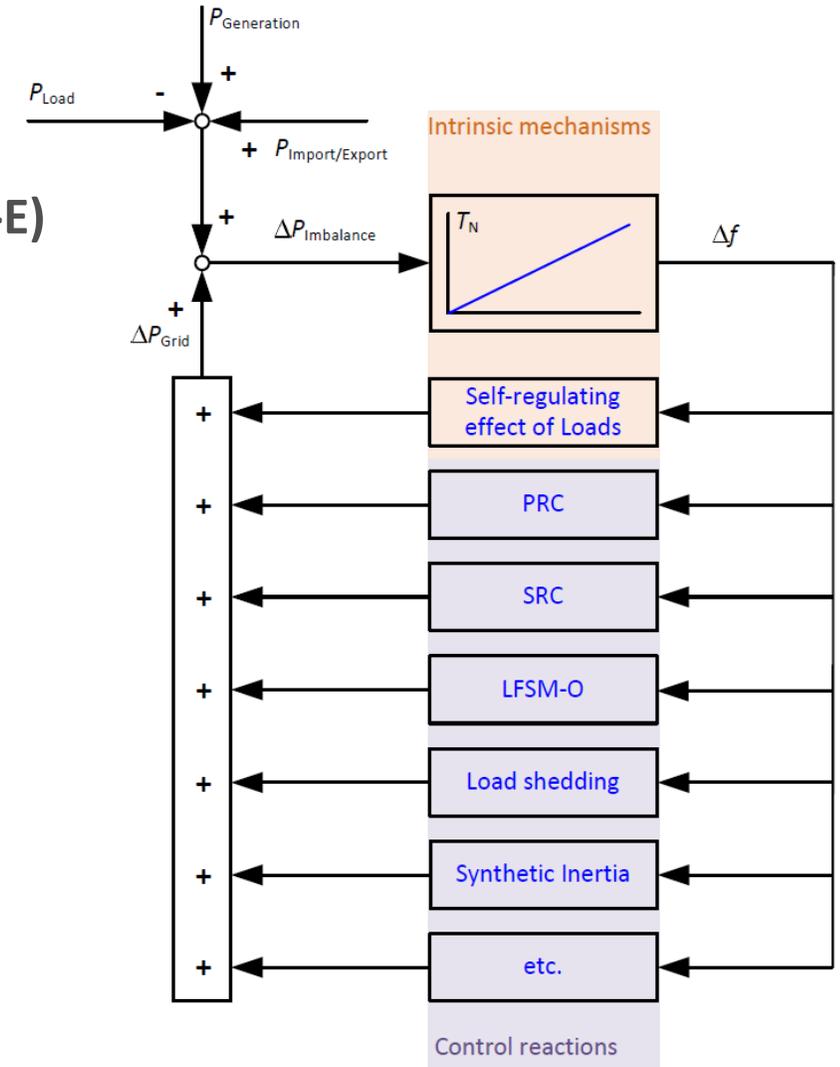
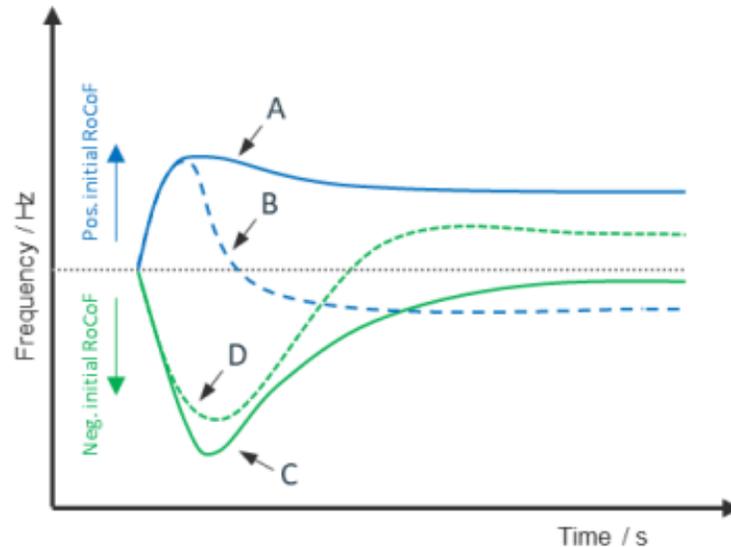


# Calculation of frequency response (f)

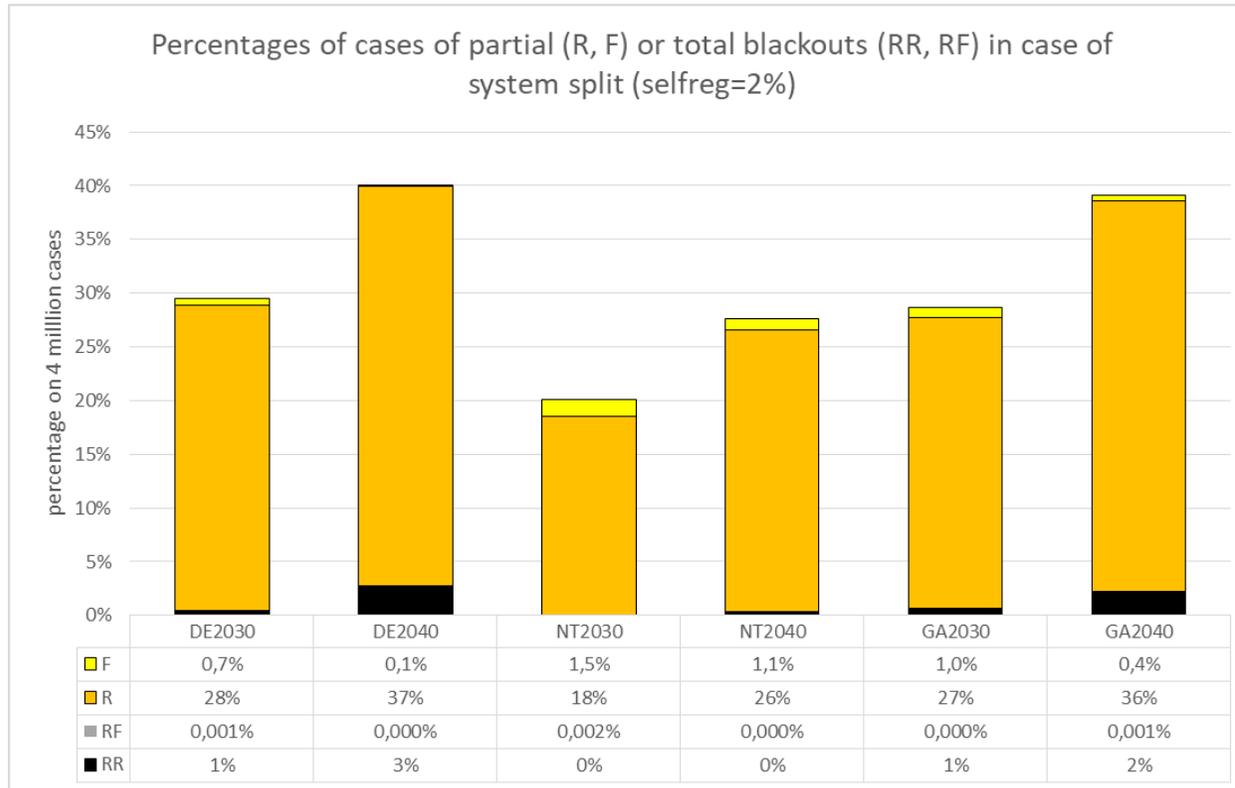
## Single Busbar model in MatLAB/Python (developed by ENTSO-E)

- Inputs per hour, split and island:
  - Imbalance (MW),
  - Inertia (MWs/MVA)

- Outputs:



# Results: algebraic RoCoF (R) and time domain simulation (f)



**RR**  
Both areas:  
 $|\text{RoCoF}| > 1\text{Hz/s}$

**RF**  
One area:  
 $|\text{RoCoF}| > 1\text{Hz/s}$   
Other area:  
 $f < \text{ or } f >$

**Total blackout**

**R**  
One area:  
 $|\text{RoCoF}| > 1\text{Hz/s}$

**F**  
One area:  
 $f < \text{ or } f >$

**Partial blackout**

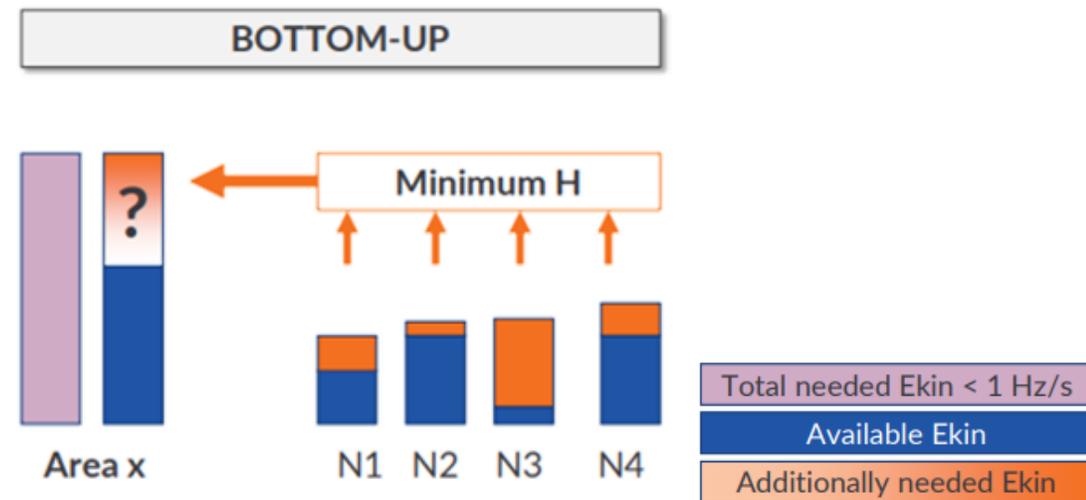
- In cases with  $|\text{RoCoF}| < 1\text{ Hz/s}$ , only few issues with frequency (RF and F cases)
- **Conclusion:**
  - RoCoF is the main issue

**→ Need to limit instantaneous RoCoF → need for foundational measures**

# Determination of mitigation measures

- Mitigation measures based on RoCoF limitation
- Calculate additionally needed kinetic energy to keep the  $|\text{RoCoF}| < 1 \text{ Hz/s}$ :

$$E_k = \frac{f_0}{2} |\Delta P| \quad \text{in GWs by hour, split and island}$$



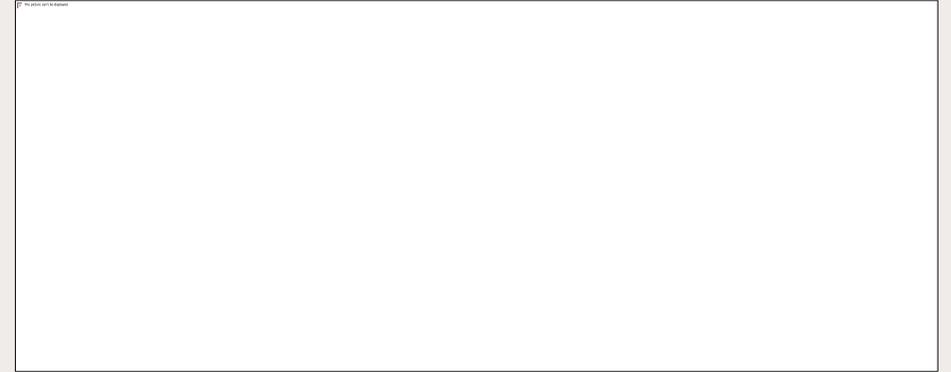
- $H_{\min}$  of **2 sMW/MVA** proposed as requirement, provides good performance:
  - # of splits satisfied
  - cost–benefit aspects

# Limitations and advantages of the approach

- In real life:
  - System splits never follow borders of market zones
  - Potentially local RoCoF >> central RoCoF
  - Impact of system split does not only depend on instantaneous response
  - Probability of system split (very low) is not considered here
- Advantages of simplified approach
  - Broad view on the phenomenon and its evolution
  - Main drivers of phenomenon captured

**Conclusion: A proper approach to assess recovery of system resilience and guarantee a good future inertia distribution**

# Minimum inertia levels

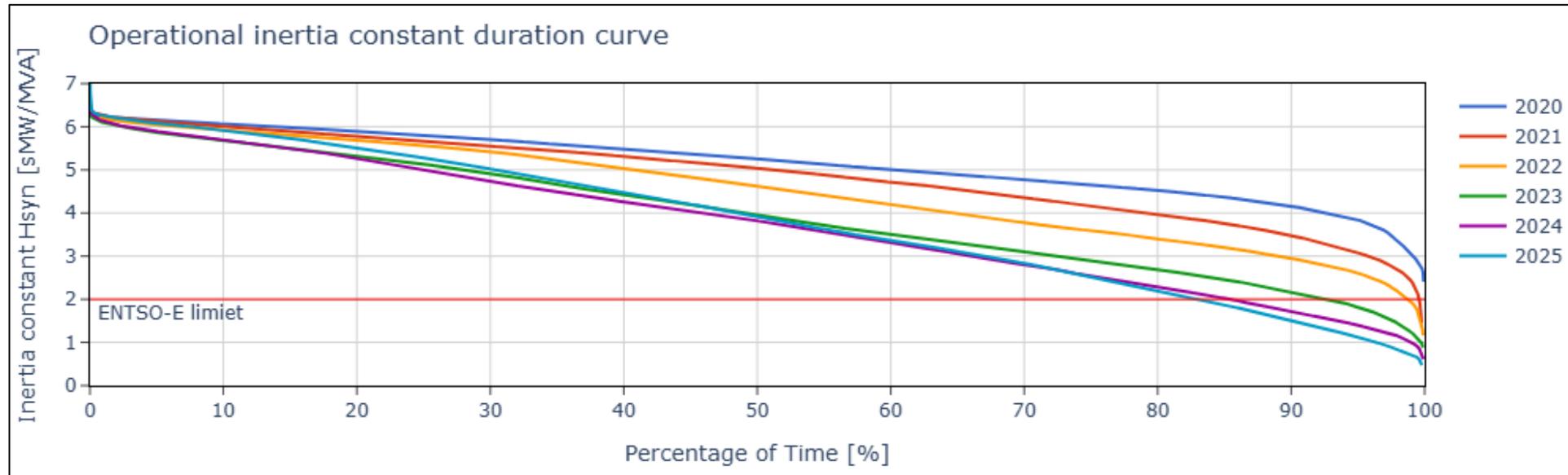


- Based on ENTSO-E Project Inertia position paper<sup>1</sup>:
  - Minimum inertia level needed per country
  - Recommended system equivalent inertia constant  $H_{\min} \geq 2 \text{ sec}$  to be ensured:
    - By **2035** (short/medium term): **50% of time** in a year
    - **Long term: 90% of time** in a year (subject to reassessment)
- On national level:
  - Absolute minimum inertia level throughout the year (GWs)
  - Threshold for the Netherlands under investigation and to be determined
    - Based on local RoCoF

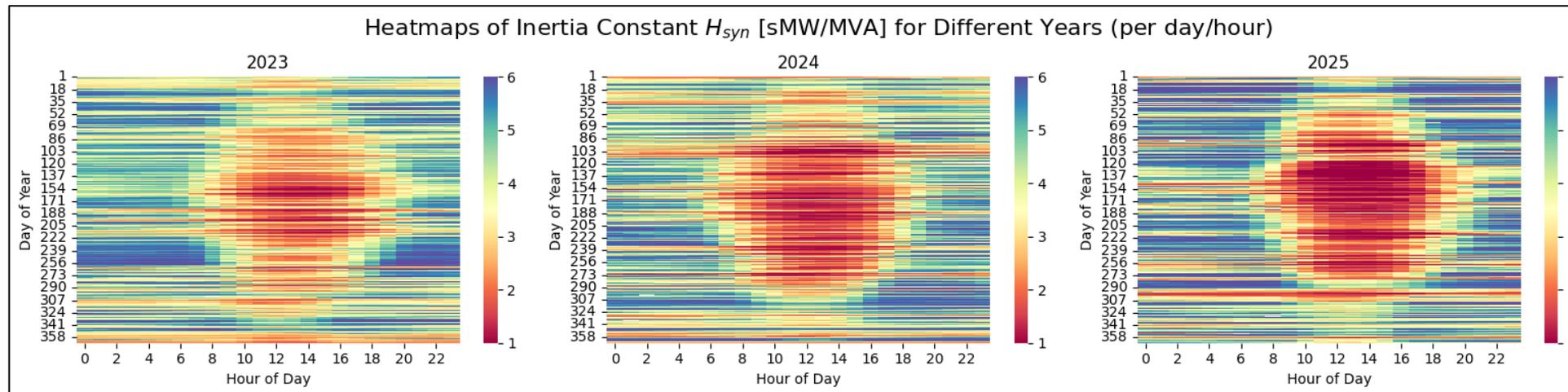


# Inertia developments in the Netherlands

# Historical inertia constant for NL

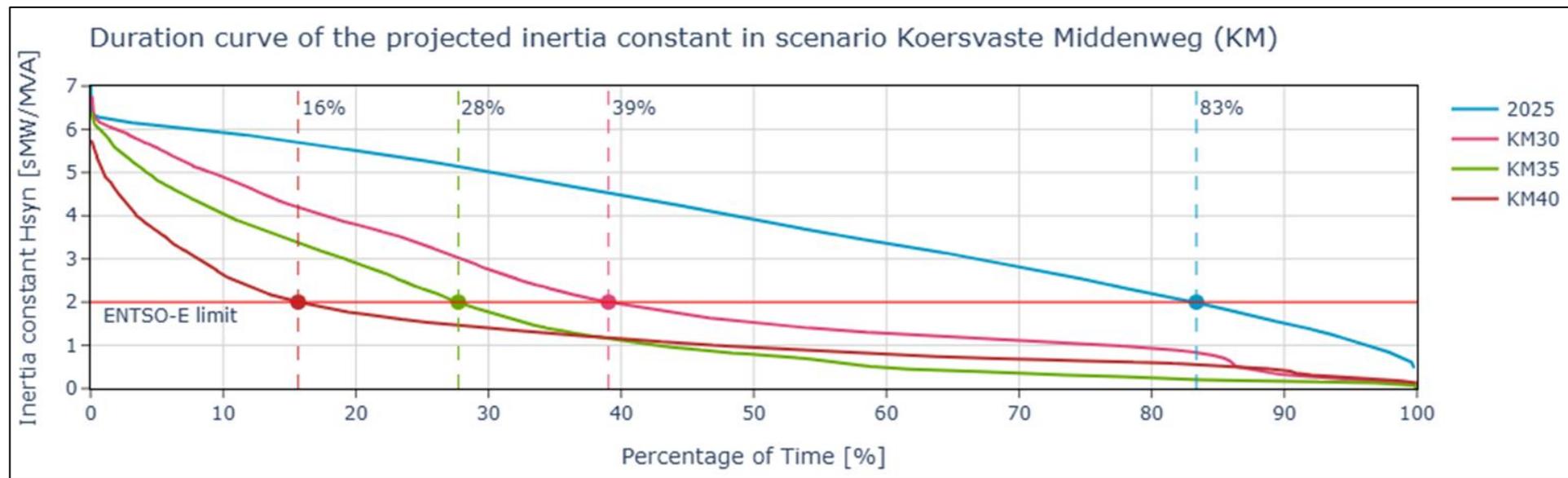


- Inertia levels are decreasing
- Still above ENTSO-E limit of  $H_{min} \geq 2s$  limit >80% if the time

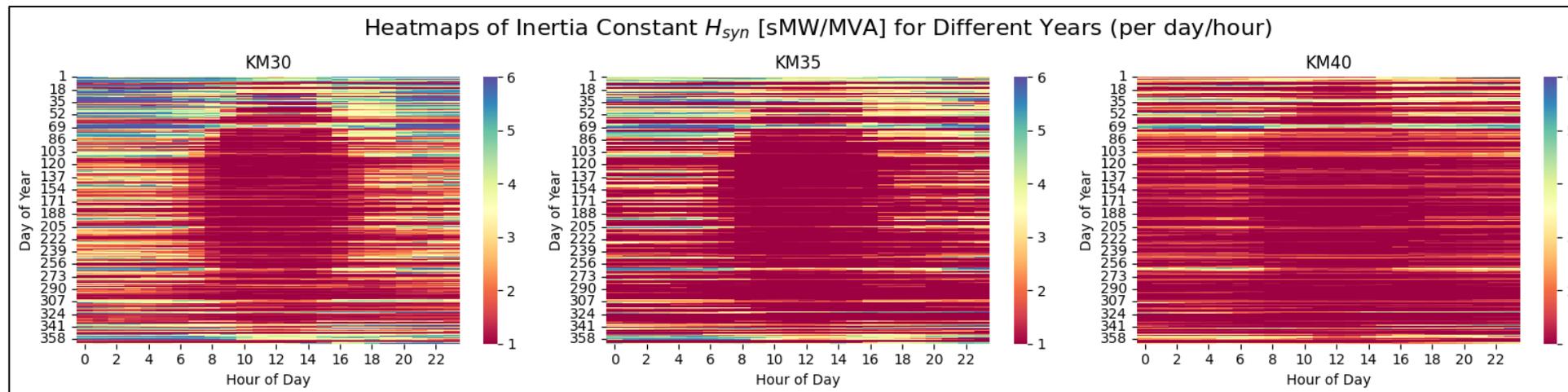


- Lowest inertia levels in summer, mid-day

# Projected future inertia constant for NL



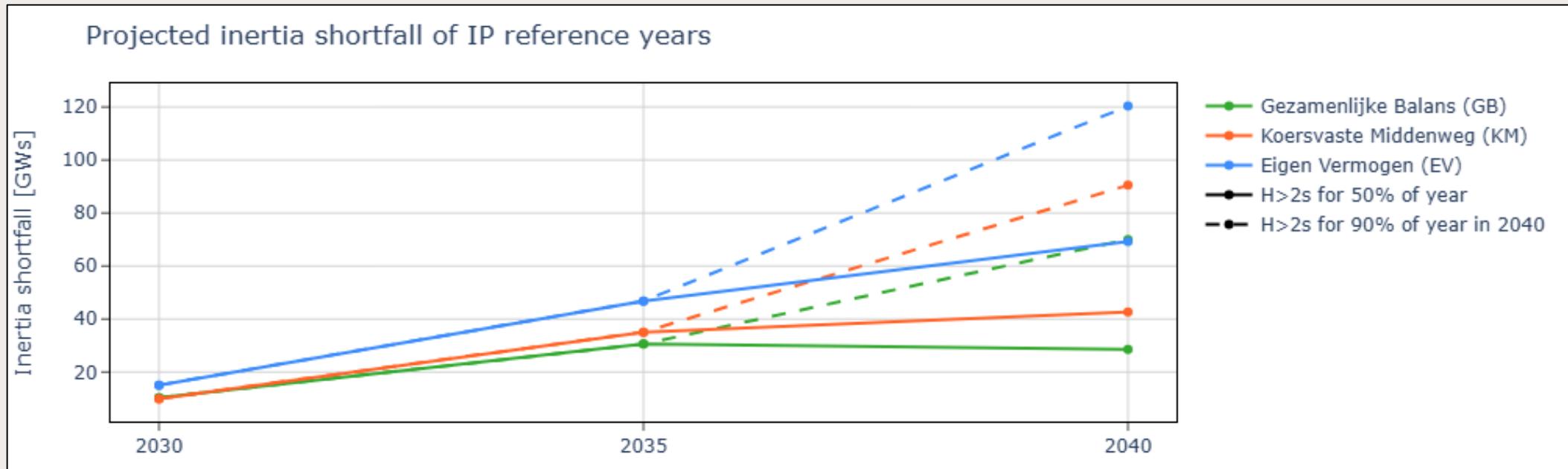
- Inertia levels are further decreasing
- Expected to drop **below** ENTSO-E limit of  $H_{\min} \geq 2s$  for 50% of the time by 2030



- Lowest inertia levels no longer only in summer, mid-day

# Inertia shortfall development

- Shortfall increases over the years
- Bandwidth and uncertainty increases further into the future

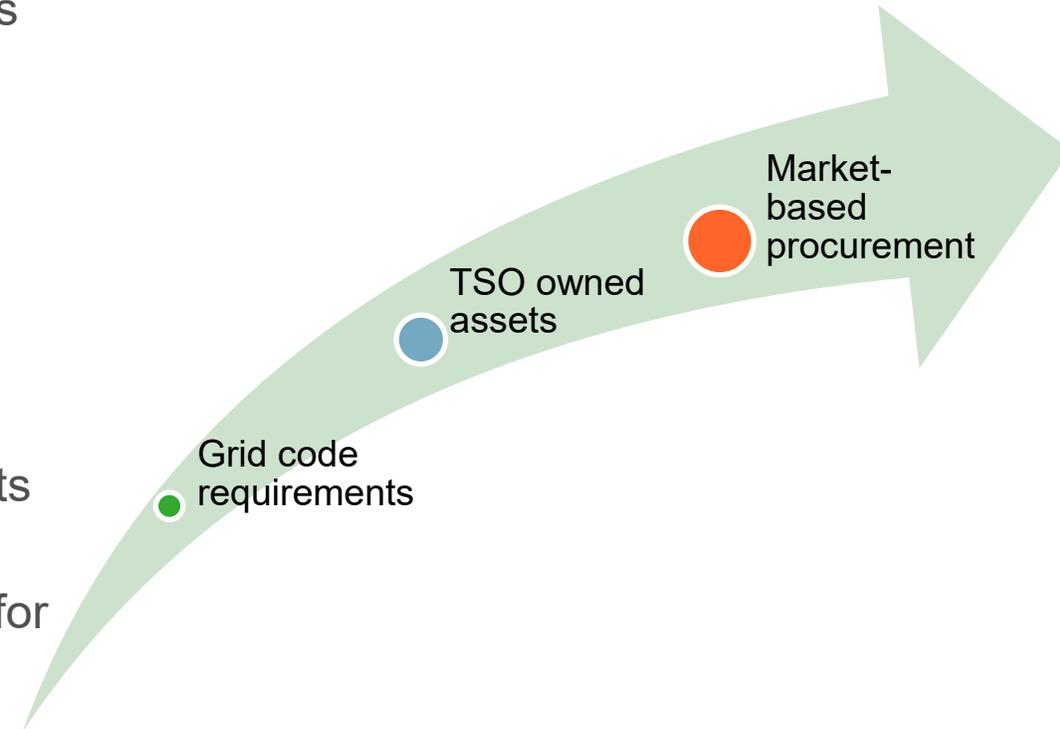


Based TenneT investmentplan 2026-2040 (IP2026) scenarios

# Currently foreseen mitigation measures

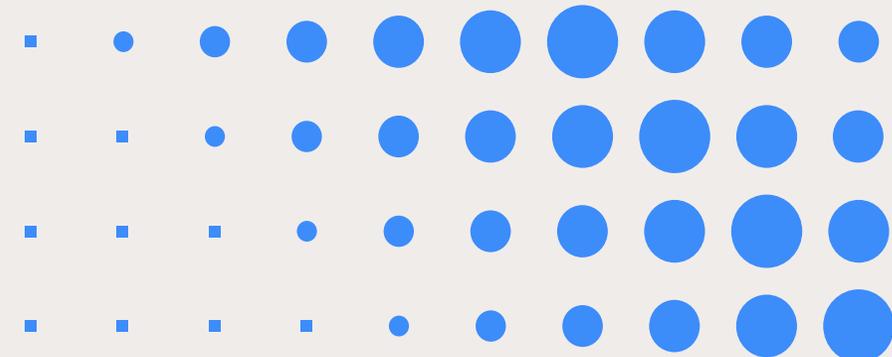
## Hybrid approach

- **Grid code requirements** to enable grid forming as a basis (inertia capability)
- **TSO owned assets**
  - Project to install three synchronous condensers
    - Improve local system strength
    - Cover part of mid-term inertia needs
  - Future project for additional 2-4 new TSO owned assets (E-STATCOM or synchronous condenser)
  - TSO owned assets only fulfill part of the inertia needs for 2035 and beyond
- **Market-based procurement**
  - Required to meet large future inertia needs



**Thank you for your attention**

**Questions?**



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## Lighting the way ahead together

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